



Measurement of In-Bore Side Loads and Comparison to First Maximum Yaw

Presented at the 29th International Symposium on Ballistics
9-13 May 2016, Edinburgh, UK



TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

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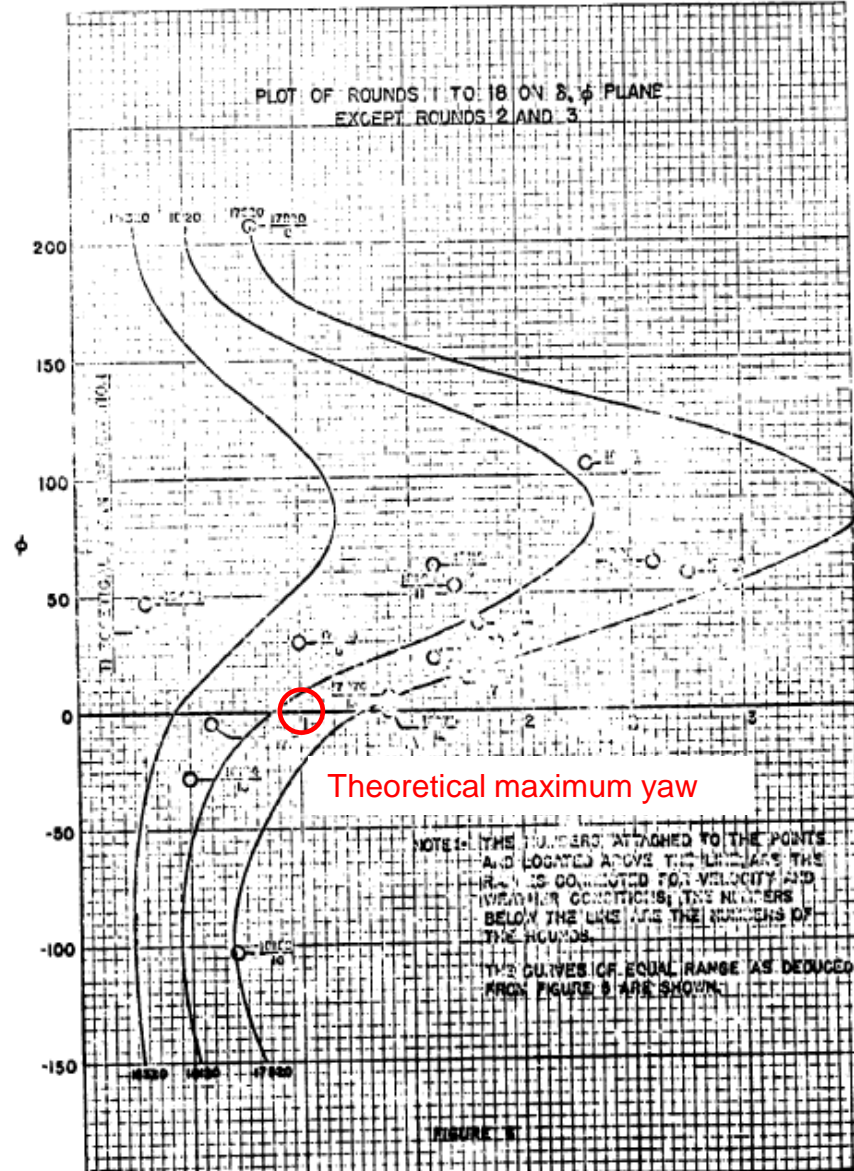
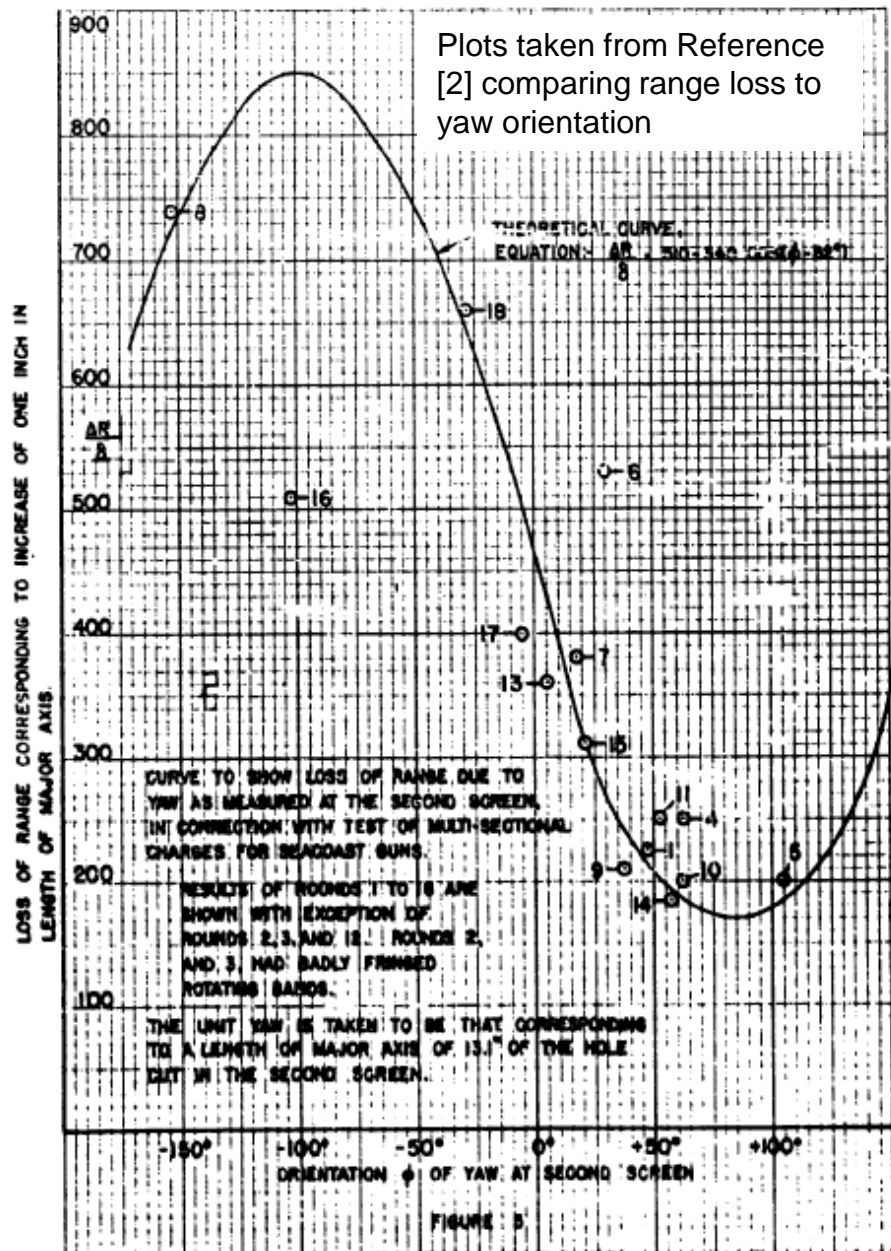
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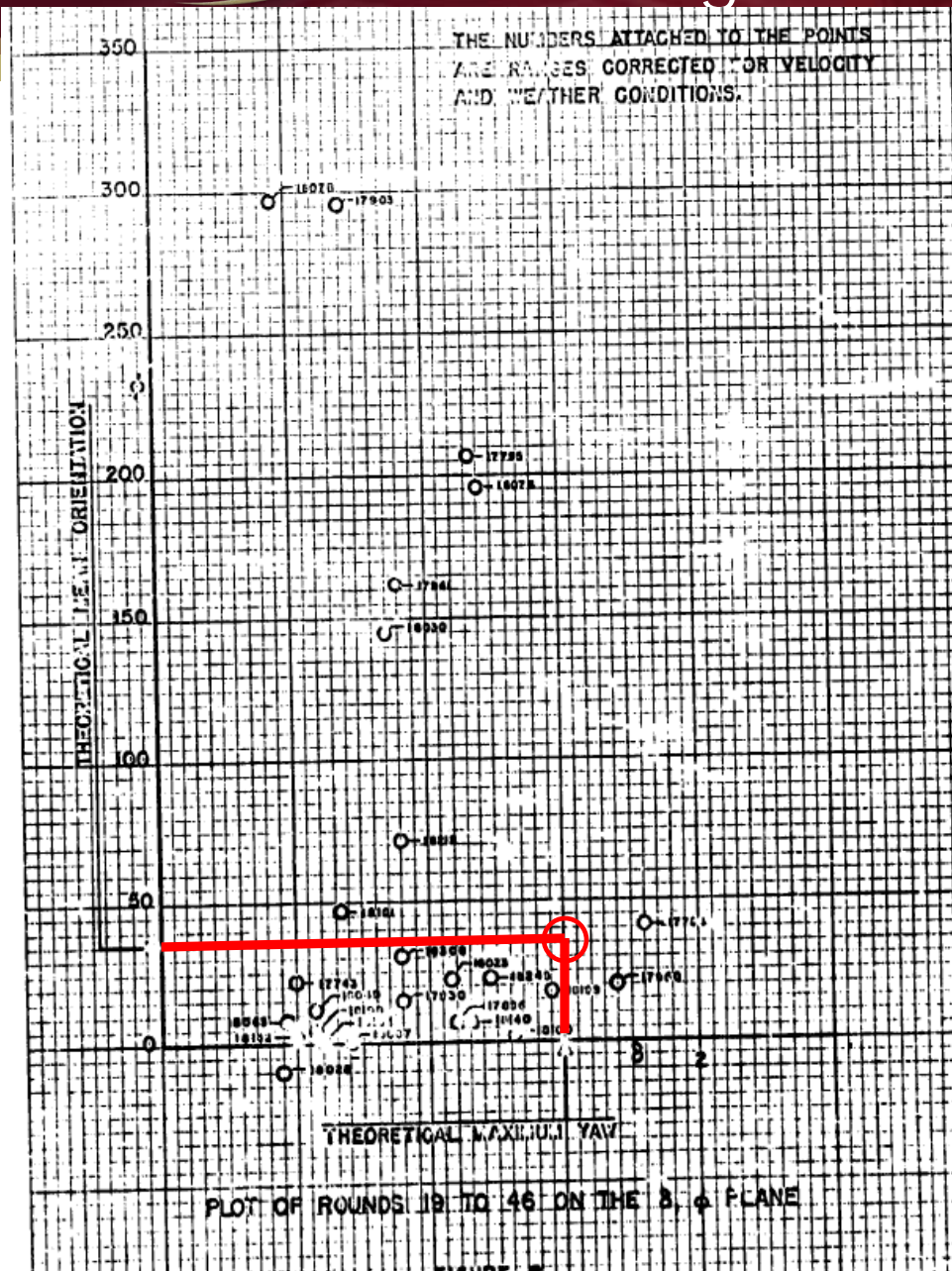
- Background
- Goal of the effort
- Approach
- Experimental set up
- Experimental results
- Analysis of results
 - Analytical
 - Statistical
- Summary and conclusions

- First maximum yaw is a good indicator of range loss in a given projectile type
 - Not all projectile designs yaw damp at the same rate
 - Projectiles of the same design should damp at the same rate and exhibit the same drag except for variations in
 - Mass distribution (design tolerances)
 - Launch disturbance
 - Down-bore motion (in-bore yaw)
 - Geometry variations (design tolerances)
 - Meteorological conditions
- The effect of bore clearance (at the muzzle) on range loss was documented in [1]
 - The more bore clearance, in general, the shorter the range to impact
- Kent, et al., documented an attempt at correlating bore clearance to range loss [2]

[1] Breger, M. P., Morrison, C. C. (Transl.). "Position and Form of Bands for Projectiles", *Notes on the Construction of Ordnance*, No. 27., Washington D. C., 10 June 1884.

[2] Kent, R. H., Hitchcock, H. P., Comparison of Predicted and Observed Yaw in Front of the Muzzle of a 12" Gun, Report No. 990 AD-116-140, USA BRL, Aberdeen Proving Ground, MD, July 1956.





$$FMY = \left(\frac{2I_T}{I_P} - 1 \right) \frac{\delta_{tm}}{\sqrt{1 - \frac{1}{S_g}}} \quad (1)$$

$$\delta_{tm} \approx \frac{d_{bore} - d}{l_{bb}} \quad (2)$$

Plots taken from Reference [2] comparing first maximum yaw to in-bore clearance

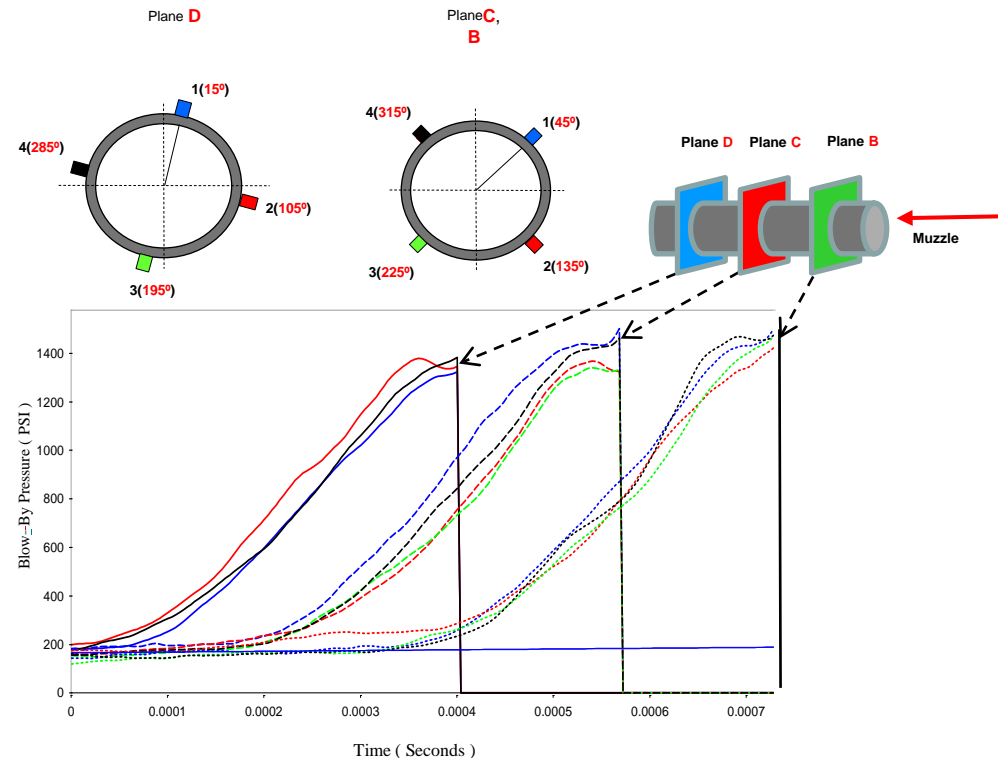
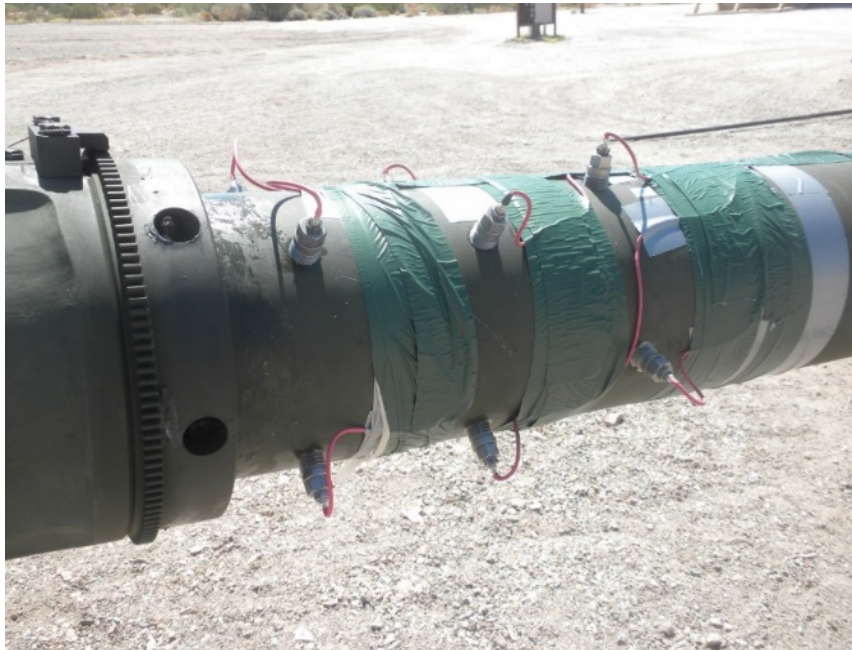
Goal of the Effort



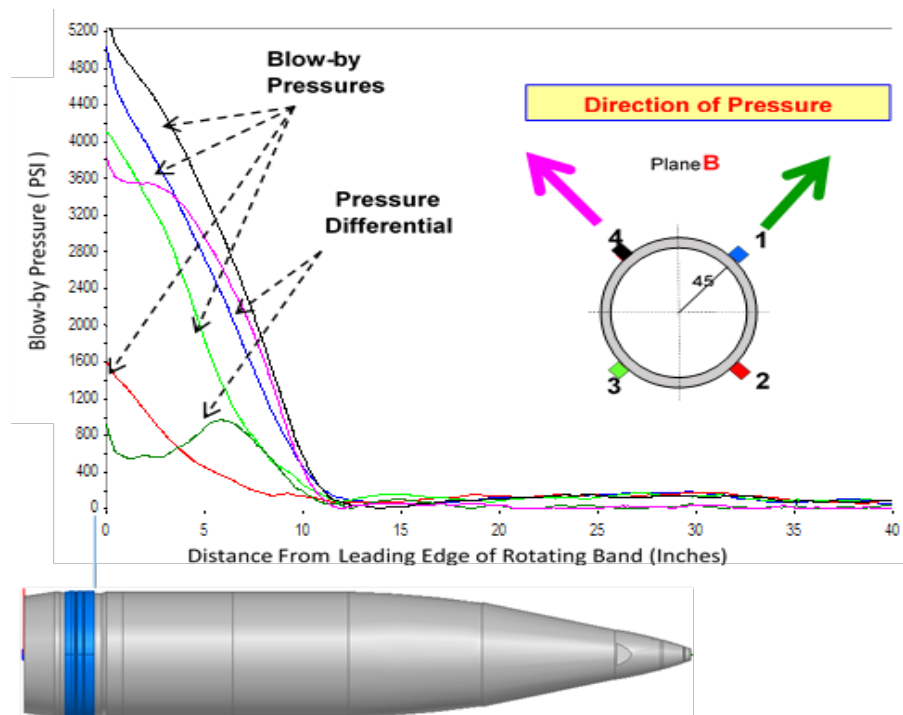
- Determine relationship between in-bore clearance and first maximum yaw
- Determine the maximum bore clearance allowable before range loss becomes unacceptable

- Through use of pressure transducers determine the force and moment acting on the projectile as it leaves the muzzle of the weapon
- In theory this should allow one to predict the magnitude and location of FMY (as well as the behavior through the rest of the flight)
- In practice it is not quite that simple
 - Weapon is moving
 - Projectile is moving
 - Finite number of pressure transducers
 - Where to put them?
 - How many is enough?
 - What do you assume for the data between transducers?
 - Axially
 - Radially
 - Gases influence outside of muzzle brake
- Knowing these limitations can we hope for a correlation?

- Gun tube structural reasons forced locations inside the tube
 - 12 transducers total
 - 3 sets of 4 (10, 15 and 20 inches from the muzzle of the weapon)
 - One set in the grooves

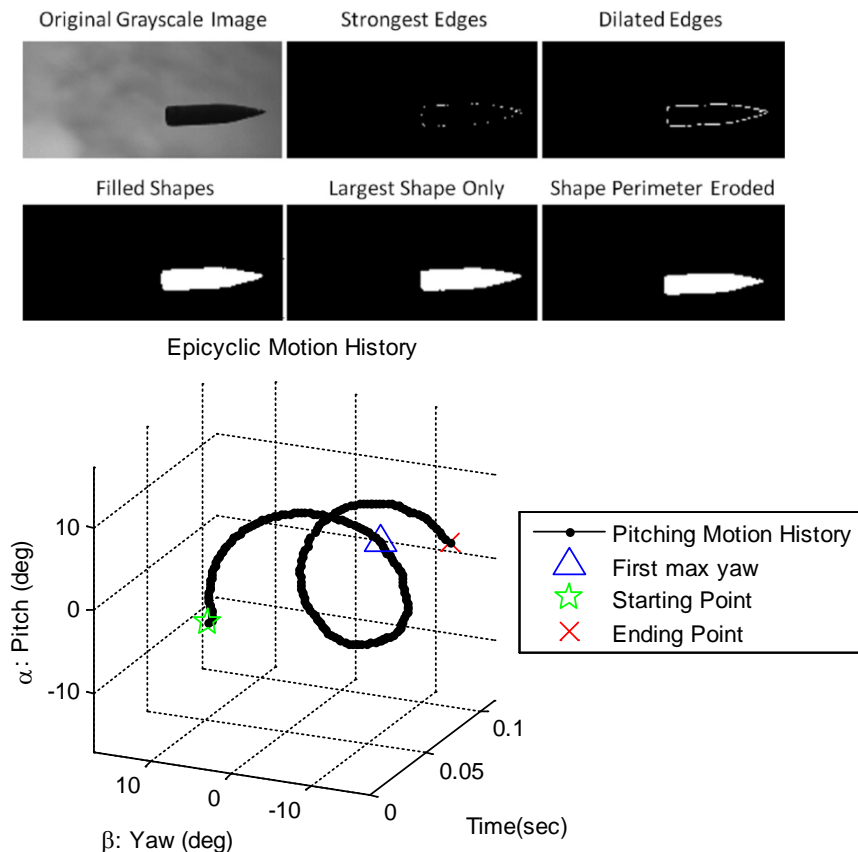


- As the projectile passes each set of transducers we obtain pressure data at that location over the time of passage
- Knowing the projectile velocity we obtain a curve looking “backwards” along the projectile length at four circumferential locations
- Assuming each of these pressures acts uniformly over a 90 degree segment we can calculate a “net”
 - Pressure force
 - Direction
 - Center of pressure
- We can now use the CG location to compute a net moment and it's direction of application

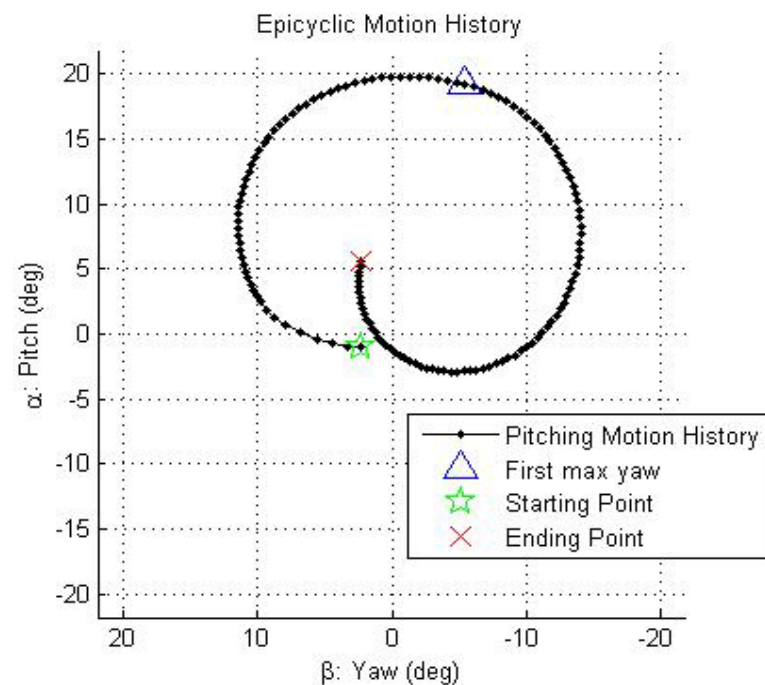


- Thus for each firing we know the applied moment
- Unfortunately this moment is applied in the tube so it's not exactly the moment that is acting on the projectile when it is free of the weapon constraints
- So if we can measure where the first maximum yaw occurs we would hope to be able to see
 - If the magnitude correlates
 - If the orientation correlates
- If this can be determined we can ask ourselves
 - Does the pressure “bubble” rotate with the rifling?

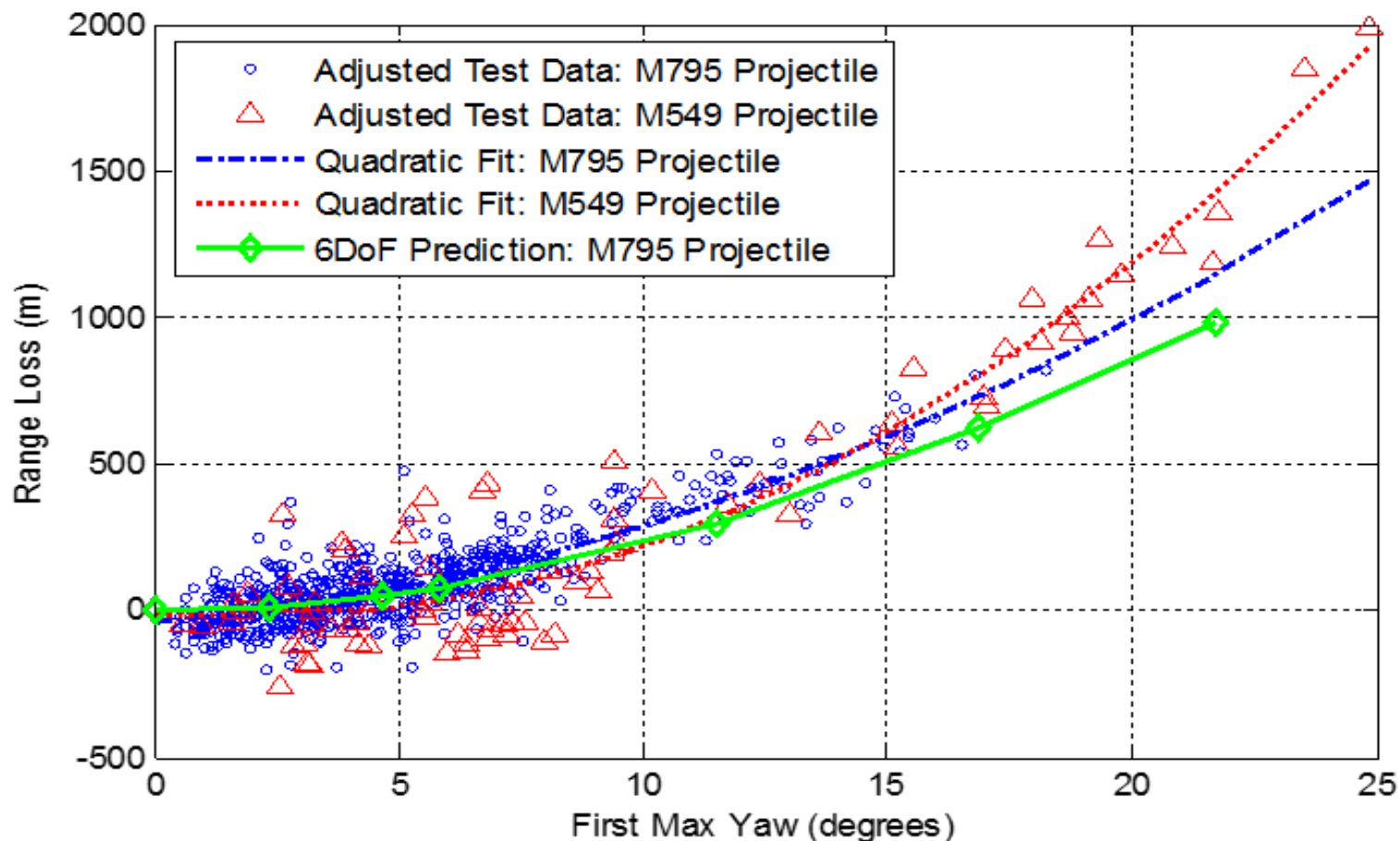
- The pressure transducer set up was depicted earlier
- The camera coverage to determine FMY consisted of two orthogonal flight follower camera systems as depicted below



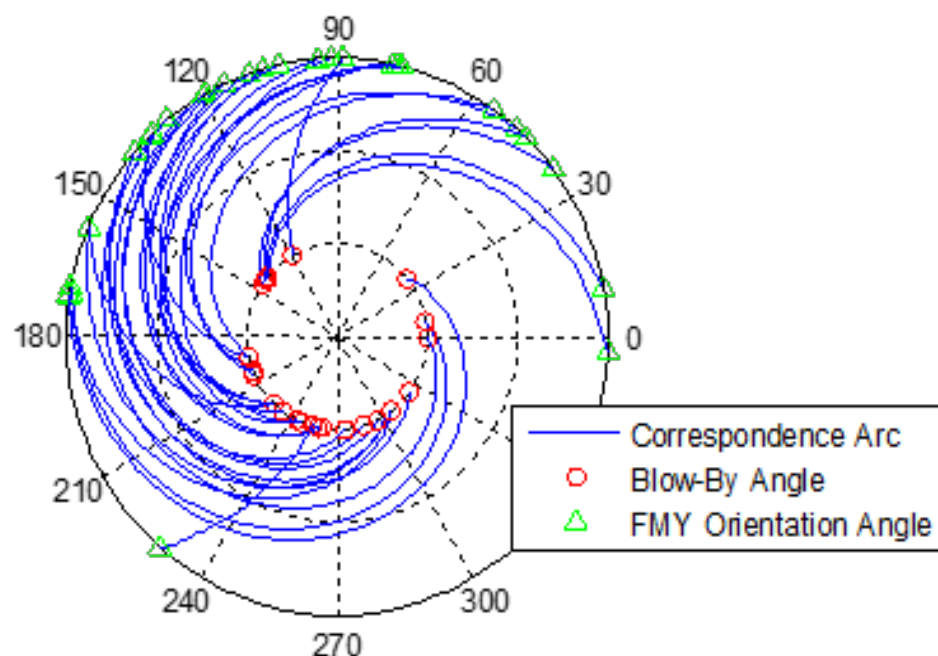
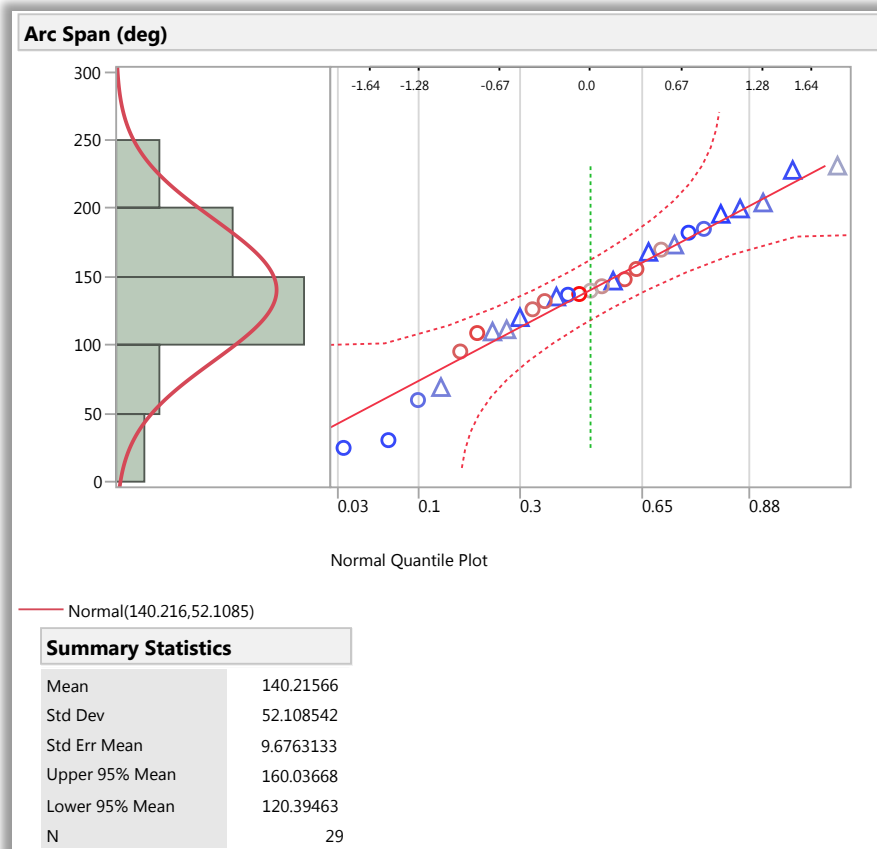
- The Automated Launch Video Analysis (ALVA) system was used to capture the projectile motion and validated against several instrumented projectiles
 - The system will be described in the paper by R. Decker
- The system was able to capture the projectile motion and determine the location and magnitude of FMY within 0.1 degrees



- The relationship between FMY and range loss was successfully observed and empirically modeled
 - This is nice and reinforced what was observed in the past



- The relationship between the magnitude and orientation of FMY and the magnitude and orientation of the net pressure force and its corresponding moment was also observed but it is noisy
 - There was a correction made for the rotation of the projectile from when the pressure data was taken



- The statistical analysis of the data showed
 - 59% of the variation in overturning moment direction in the tube was explained by 'blow-by angle'
 - 41% of the data did not and is attributed to the other suspected but unquantified sources of variation
 - Weapon is moving during and after measurement
 - Projectile is moving during and after measurement
 - Finite number of pressure transducers
 - Where they were
 - How many we had
 - How we integrated between them
 - Gases influence outside of muzzle brake
 - Others?
 - Different projectiles behaved differently
 - M549: 76% of variation explained by overturning torque
 - M795 : 24% of variation explained by overturning torque
 - Geometry related?

- First Maximum Yaw (Still) is directly related to range loss
- In-Bore moments caused by blow-by affect FMY
 - Differently for different projectiles
 - Other factors are at work
- Accurate measurements of FMY can be obtained by video means (more in the Decker paper)
- Although no future work is currently planned by ARDEC to delve more deeply into this topic there are still a great many questions that need to be answered

Questions?